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- Sakagami, Seigou,
c/o Itami Works
Itami-shi, Hyogo (JP)
- Ibuki, Masanori,
c/o Itami Works
Itami-shi, Hyogo (JP)
- Kishimoto, Hiroya,
c/o Itami Works
Itami-shi, Hyogo (JP)

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(71) Applicant: Sumitomo Electric Industries, Ltd.
Osaka 541 (JP)(72) Inventors:

- Nitto, Fumiaki,
c/o Itami Works
Itami-shi, Hyogo (JP)
- Sano, Tatsuya,
c/o Itami Works
Itami-shi, Hyogo (JP)

(74) Representative: Eder, Eugen, Dipl.-Ing.
Patentanwälte
Dipl.-Ing. E. Eder
Dipl.-Ing. K. Schieschke
Elisabethstrasse 34
D-80796 München (DE)

(54) Non-asbestos friction material

(57) A non-asbestos friction material containing a reinforcing fiber other than asbestos, organic fillers, friction adjusting ingredients, and a thermosetting resin for binding the reinforcing fiber, the organic fillers and the friction adjusting ingredients together. The friction adjusting ingredients contain magnesia in the form of secondary particles which are an aggregate of primary particles. The use of magnesia in the form of secondary particles reduces low-frequency noise and squeak while keeping the attack on the mating member low and keeping high the resistance to fading and the coefficient of friction.

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Description

The present invention relates to a friction material for use as automotive disk brake pads and brake linings, and particularly a non-asbestos friction material which produces less low-frequency noises during braking, while keeping its low attack to the mating member and its high fade resistance and friction coefficient.

Asbestos pads are now being rapidly replaced by non-asbestos ones. One problem with such non-asbestos pads is that they tend to produce low-frequency noises during braking.

One way to reduce such noises is to rub off any deposits on the surface of the disk rotor, which are the main cause of such noises, by adding an abrasive having a Moh's hardness of not less than 6 to the friction material. Another way is, as disclosed in Unexamined Japanese Patent Publication 4-60225, to add a flaky inorganic substance having self-shearing lubricating properties such as mica and talc to the friction material. By adding such a substance, the mating member can slide smoothly on the friction member even while the surface pressure is high, at which time low-frequency noises tend to be produced. Thus, it is possible to prevent stick slip, which is the major cause of low-frequency noises.

Another solution, which is proposed in Unexamined Japanese Patent Publication 5-32965, is to add a non-metallic inorganic substance having a Moh's hardness between 3 and 9 and an inorganic hydrate having a Moh's hardness not exceeding 5 in predetermined amounts, while reducing the carbon content.

In the method in which deposits on the surface of the rotor are removed by adding an abrasive to the friction member, the abrasive has to have a sufficiently large particle size. But the larger the particle size of the abrasive, the more severely the friction member tends to attack the rotor. This leads to local increase in the surface pressure during braking. Such locally high surface pressure may cause streaks on the surface of the rotor, which tends to destabilize the braking effect and increase squeaks (high-frequency noise) during braking.

In the method in which a flaky inorganic substance such as mica or talc is added, due to crystal structure of the inorganic substance used, the friction coefficient (hereinafter referred to as μ) tends to be low, so that the resistance to fading drops. It is also known that if an abrasive having a large particle size is added to the friction material in an attempt to increase μ , the resistance to fading drops markedly for unknown reasons.

In the technique proposed in Unexamined Japanese Patent Publication 5-32956, by reducing the carbon content, it is possible to suppress the production of substances that form a film deposit. Also, the hydrate added serves to prevent the film forming substances from adhering to the surface of the rotor. Moreover, the inorganic substance having a Moh's hardness of 3-9 removes any deposits on the rotor surface. But since the hydrate has a low Moh's hardness, μ tends to be low. Also, the hydrate presumably causes a drop in the wear resistance of the friction material.

Further, if the inorganic substance having a high Moh's hardness is too high in particle size, the rotor tends to be worn unevenly. If too low, deposits cannot be removed effectively.

The applicant of this invention also proposed in Unexamined Japanese Publication 62-15281 to add 8-12% by volume of magnesium oxide powder having a maximum particle diameter not exceeding 250 μm in order to increase μ . Since the magnesium oxide has a high Moh's hardness, it acts as an abrasive. But if its particle size is too large, the friction member tends to more severely attack the mating member. If too small, it cannot remove deposits effectively.

In short, none of these conventional methods can suppress low-frequency noise without worsening any of the other properties of the friction material.

An object of the present invention is to provide a high-performance, non-asbestos friction material which produces less low-frequency noises while keeping low its tendency to attack the rotor, its high fade resistance and high μ .

According to the present invention, there is provided a non-asbestos friction material comprising a reinforcing fiber other than asbestos, organic fillers, friction adjusting ingredients, and a thermosetting resin for binding the reinforcing fiber, the organic fillers and the friction adjusting ingredients together, the friction adjusting ingredients containing magnesia in the form of secondary particles, which are an aggregate of primary particles.

The secondary particles of magnesia should be aggregates of primary particles having diameters not exceeding 0.5 μm and preferably have a diameter between about 1 and 5 μm .

Preferably, the content of the secondary particles of magnesia should be 3-20% by volume of the entire friction material.

The reinforcing fibers are conventional and may be one or more than one kind of fibers selected from the group consisting of organic fibers such as alamide, acrylic, carbon and phenolic fibers, inorganic fibers such as glass, alumina, silicate and rock wool fibers, steel fibers, stainless steel fibers, copper fibers, and copper alloy fibers such as brass fibers.

The organic filler may be one or more than one selected from cashew dust, melamine dust, NBR powder and SBR powder.

The friction adjusting ingredient may be magnesia and one or a combination selected from lubricants such as molybdenum disulfide, antimony trisulfide and graphite, abrasives such as alumina, zirconium oxide, zirconium silicate, silica or rutile, metallic powders such as copper, aluminum, zinc and tin powders, and inorganic substances such as barium sulfate, calcium carbonate and calcium hydrate.

Further, the friction material contains as a binder one or more than one thermosetting resin selected e.g from phenolic, melamine, polyimide and epoxy resins.

Magnesia is available in two forms, i.e. one manufactured by drying and calcining magnesium hydroxide, and one manufactured by electromelting and pulverizing magnesium hydroxide. The magnesia used in the present invention is the former type. It should preferably be the one obtained by calcining at about 1000 °C.

Magnesia is a hard material having a Moh's hardness of 6. In the present invention, magnesia is added in the form of secondary particles. With this arrangement, it is possible to increase the diameters of the secondary particles to a suitable level so that deposits on the rotor surface can be removed effectively, while suppressing the production of low-frequency noises.

Secondary particles, i.e. aggregates of primary particles, are lower in strength than non-aggregated primary particles. Namely, they are easily deformed under a certain degree of pressure due to the peeling of primary particles forming the secondary particles. Thus, no local increase in the surface pressure occurs, so that friction vibrations that cause squeaks are less likely to happen. Since the surface pressure is evenly distributed, the rotor is less likely to suffer uneven wear, so that braking effects will remain stable.

Since the secondary particles collapse easily under a certain degree of pressure, the magnesia is in the form of small-diameter primary particles at the interface with the rotor. Thus, the attack on the mating member (rotor) is kept sufficiently low. Since the friction material according to the present invention contains no flaky inorganic substances, its μ and resistance to fading are sufficiently high. Since the addition of magnesia never leads to intensified attack on the mating member, it is possible to increase the content of magnesia to a considerable degree. This also leads to increased μ .

By adding the magnesia in the form of secondary particles, which are aggregates of primary particles, to the friction material according to the present invention, it can remove deposits on the rotor as effectively as a conventional abrasive having large particle diameter, while suppressing the attack on the rotor to a minimum. In short, by adding magnesia, the friction coefficient increases to a sufficient level and stabilizes, the resistance to fading increases, the attack on the mating member decreases, and low-frequency noises and squeaks are less likely to be produced.

If the secondary particles of magnesia are too small in diameter, they can scarcely suppress low-frequency noises. If too large, the brake tends to squeak. If the primary particles are too large in diameter, the attack on the mating member will intensify.

We have confirmed by experiments that by using magnesia having a primary particle diameter of 0.5 μm or lower and a secondary particle diameter of 1.5 μm , it is possible to sufficiently suppress low-frequency noises while keeping the attack on the mating member and the squeaks to sufficiently low levels. The diameter of the primary particles is correlated to the calcining temperature of magnesium hydroxide. Namely, the higher the calcining temperature, the larger the primary particle diameter and the harder the magnesia obtained. We set the upper limit of the primary particle diameter at 0.5 μm partly because primary particles having a diameter larger than 0.5 μm tend to be too hard. But the real reason therefor is related to the manufacture of secondary particles of magnesia. Namely, primary particles of magnesia are easily aggregated into the form of secondary particles at temperatures which can give primary particles having diameters not exceeding 5 μm , whereas at temperature higher than the above range, no secondary particles are formable.

The higher the content of the secondary particles of magnesia in the friction material, the more effectively it is possible to reduce low-frequency noises and increase μ . But the smaller the content, the lower the attack on the mating member and the higher the resistance to fading. In order to improve all these properties in a balanced manner, we determined that the content of such magnesia should be 3-20% by volume.

Examples of the present invention are now described.

Disk brake pads for use in automobiles as Examples 1-11 and Comparative Examples 1-4 were prepared using materials having the composition shown in Tables 1 and 2. For each pad, we measured the low-frequency noise level, squeak level, friction coefficient (μ), resistance to fading, and attack to the mating member. Particle diameters in the tables are average values. Secondary particles shown in the tables are all aggregates of primary particles having a diameter of 0.5 μm or less.

Reinforcing fibers used in any of Examples and Comparative Examples were a combination of aromatic polyamide fibers, slug wool fibers and copper fibers.

Also, we used cashew dust and NBR powder as the organic filler, a phenolic resin as the binder, and graphite, molybdenum disulfide, barium sulfate, and calcium hydroxide as the friction adjusting ingredients.

As shown in the tables, the components from the aromatic polyamide to the calcium hydroxide are identical both in the kind and volume percentage in all of the Examples and Comparative Examples, with only the kind and content of the magnesium oxide (magnesia) being different from one another. Example 7 and Comparative Example 3 further contain mica. The difference in the overall volume among the specimens due to the difference in the volume percentages of these components were adjusted by adding different amounts of barium sulfate.

The pad samples were manufactured with a known molding technique. Specifically, the material powders mixed in the ratios shown in Tables 1 and 2 were pre-formed under the pressure of 300 kg/cm² at normal temperature, and then pressurized while degassing at 400 kg/cm² in a mold heated to 160 °C. The articles thus formed were heated for five

hours at 230 °C for after-curing of the phenolic resin, and then grinded to a predetermined thickness to obtain the pad samples.

Various properties of the brake pads thus obtained were measured in the following manner.

5 1) Measurement of low-frequency noises and squeaks

Each pad samples was fitted on a vehicle (automatic-transmission passenger car with a 2000 cc engine) and the car was started and stopped under the conditions shown in the noise confirmation matrix in Table 3, while the driver checked if he heard low-frequency noises and/or squeaks when the car was started and stopped. The corresponding figures in Tables 1 and 2 represent the percentages of the number of times the driver heard low-frequency noises and squeaks, respectively

2) Measurement of friction coefficient and fade min μ

15 These properties were measured using a brake dynamometer under the test code JASO C406-82 and under the conditions of: caliper: floating type (cylinder area 20.4 cm²), inertia: 5 kg.m.S², tire radius: 0.280 m, effective braking radius: 0.094 m, disk rotor diameter: 0.238 m, disk rotor thickness: 18 mm (ventilated type).

20 3) Measurement of the attack on the mating member

25 This test was conducted using a brake dynamometer under the conditions of: rotor temperature before braking: 50 °C, initial velocity: 50 km/hr, deceleration: 0.3g, the number of time the brake is applied: 1000. After the test, the amount of wear of the rotor was measured. Other test conditions were the same as those in the test 2).

The results of this test are shown in Tables 1 and 2.

30 As will be apparent from the results for Examples 1-6 in Table 1, the higher the content of the secondary particles of magnesia, the less low-frequency noises are likely to be produced. From the result of Example 7, it is apparent that the addition of mica further strengthens the noise-suppressing effect.

35 The value μ also tends to increase with the content of magnesia. In contrast, the fade min μ tends to drop as the content of magnesia increases. The attack on the rotor is supposed to increase as the content of magnesia increases. But in the present invention, by using the secondary particles of magnesia, the attack on the rotor intensified little even when the content of magnesia is increased. For example, there is a big difference in the attack level on the mating member between Examples 1 and 3 on the one hand and Comparative Examples 1 and 2 on the other, in spite of the fact that the content and the particle diameter of the magnesia added are the same.

40 Comparative Examples 1-3 shown in Table 2 contain magnesia obtained by electromelting and not in the form of secondary particles. That is, the magnesia consists of discrete primary particles. At particle diameter of about 2 μm , they cannot suppress low-frequency noises at all. On the other hand, Examples according to the present invention can reduce low-frequency noises markedly even if its primary particle diameters are small. The smaller the primary particle diameters, the smaller the secondary particle diameters, so that the less the brake is likely to squeak and the lower the attack on the rotor. Although magnesia formed by electromelting can increase the μ value more effectively, it is apparent that magnesia in the form of secondary particles can more effectively increase the resistance to fading, suppress squeaks and lower the attack on the rotor. As for the resistance to fading, the difference is particularly big between the materials containing mica (Example 7 and Comparative Example 3). Thus, it is more advantageous to use magnesia in the form of secondary particles than magnesia obtained by electromelting if mica is added to reduce low-frequency noises.

45 Examples 8-11 were prepared to see what influence the diameter of the secondary particles of magnesia has on various properties of the friction material. No significant difference in performance is seen while the secondary particle diameters of magnesia are within the range of 1-5 μm . But Example 10, whose secondary particle diameter is 0.7 μm , produced a rather high level of low-frequency noises. Example 11, having a secondary particle diameter of 7 μm , squeaked a little louder.

50 Similar phenomena were also observed where the content of secondary particles of magnesia is less than 3% by volume (Example 1) or more than 20% by volume (Example 6).

The preferable ranges of the diameter and content of the secondary particles of magnesia were determined taking these results into consideration.

55 The combinations of components mentioned in Examples are mere examples. The abovementioned various benefits of the present invention may be obtained with other combinations of the components listed in Table 3 and/or with the secondary particles of magnesia added in a different amount.

As described above, the friction member according to the present invention contains magnesia, a substance capable of effectively removing deposits on the rotor surface and increasing μ , in the form of secondary particles, or aggregates of primary particles. Thus, it is possible to reduce low-frequency noises without worsening other properties. Thus, according to the present invention, there is provided a high-performance non-asbestos friction material which is low in the attack

on the mating member, high in the resistance to fading, and less likely to cause uneven wear of the rotor, squeaks and low-frequency noises.

[Table 1]

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	Component/No	Examples										
		1	2	3	4	5	6	7	8	9	10	11
Material (vol %)	Aromatic polyamide fiber	15	15	15	15	15	15	15	15	15	15	15
	Rock wool	5	5	5	5	5	5	5	5	5	5	5
	Copper fiber	5	5	5	5	5	5	5	5	5	5	5
	Cashew dust	15	15	15	15	15	15	15	15	15	15	15
	NBR powder	5	5	5	5	5	5	5	5	5	5	5
	Phenol resin	20	20	20	20	20	20	20	20	20	20	20
	Graphite	5	5	5	5	5	5	5	5	5	5	5
	Molybdenum sulfate	2	2	2	2	2	2	2	2	2	2	2
	Calcium hydroxide	2	2	2	2	2	2	2	2	2	2	2
	Barium sulfate	25	23	21	16	6	1	6	16	16	16	16
Magnesium oxide	Mica							10				
	Secondary particle	2 μm	1	3	5	10	20	25	10			
		1 μm							10			
		5 μm								10		
		0.7 μm									10	
		7 μm										10
		Electro melt	2 μm									
Property	Low-frequency noise (%)	6.2	2.2	2.1	1.5	1.3	1.1	0.3	1.3	1.4	5.9	1.8
	Squeak (%)	0	0	0	0	0	3.3	0	0	0	0	4.3
	Friction coefficient (μ) Deceleration 0.6g	20 km/h	0.35	0.37	0.38	0.40	0.42	0.45	0.40	0.40	0.41	0.39
		50	0.33	0.35	0.36	0.37	0.39	0.41	0.37	0.38	0.39	0.37
		100	0.36	0.38	0.38	0.40	0.40	0.43	0.38	0.39	0.40	0.39
		130	0.31	0.32	0.32	0.35	0.35	0.37	0.33	0.34	0.36	0.34
	Fade min μ	0.25	0.25	0.25	0.24	0.22	0.19	0.22	0.24	0.25	0.23	0.22
	Rotor attack μm	1	2	2	3	4	6	3	3	3	2	4

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[Table 2]

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	Material (vol %)	Component/No	Examples			
			1	2	3	4
Aromatic polyamide fiber	Magnesium oxide	Aromatic polyamide fiber	15	15	15	15
		Rock wool	5	5	5	5
		Copper fiber	5	5	5	5
		Cashew dust	15	15	15	15
		NBR powder	5	5	5	5
		Phenol resin	20	20	20	20
		Graphite	5	5	5	5
		Molybdenum sulfate	2	2	2	2
		Calcium hydroxide	2	2	2	2
		Barium sulfate	25	21	11	26
Secondary particle	Friction coefficient Deceleration 0.68	Mica			10	
		2 μm				
		1 μm				
		5 μm				
		0.7 μm				
		7 μm				
Property	Electro melt	2 μm	1	5	5	
		Low-frequency noise (%)	9.5	13.5	5.6	15.9
	Squeak (%)		5.8	7.9	8.5	2.5
	Friction coefficient Deceleration 0.68	20 km/h	0.39	0.42	0.40	0.34
		50	0.37	0.39	0.38	0.33
		100	0.39	0.38	0.37	0.34
		130	0.34	0.32	0.30	0.29
	Fade min μ		0.21	0.19	0.13	0.25
	Rotor attack μm		7	9	10	1

[Table 3]

	Pad temp before braking (°C)	Initial speed (km/hr)	Deceleration (g)	Braking number of times (time)	Braking interval (m)
1 Noise check matrix	1 0 0, 1 5 0 2 0 0, 2 5 0	5 0	0. 1, 0. 3 0. 5, 0. 7	1 each	
2 Rubbing	1 0 0	6 5	0. 3 5	2 0 0	
3 Noise check matrix	1 0 0, 1 5 0 2 0 0, 2 5 0	5 0	0. 1, 0. 3 0. 5, 0. 7	1 each	
4 Fade	6 5 (first) time	1 0 0	0. 4 5	1 5	6 5 0
5 Noise check matrix	1 0 0, 1 5 0 2 0 0, 2 5 0	5 0	0. 1, 0. 3 0. 5, 0. 7	1 each	

Claims

50 1. A non-asbestos friction material comprising a reinforcing fiber other than asbestos, organic fillers, friction adjusting ingredients, and a thermosetting resin for binding the reinforcing fiber, the organic fillers and the friction adjusting ingredients together, said friction adjusting ingredients containing magnesia in the form of secondary particles, which are an aggregate of primary particles.

55 2. A non-asbestos friction material claimed in claim 1 wherein said secondary particles of magnesia are an aggregate of primary particles having a diameter not exceeding 0.5 µm and having a diameter between 1 and 5 µm.

3. A non-asbestos friction material claimed in claim 1 or 2 wherein the content of said secondary particles of magnesia is 3-20% by volume of the entire friction material.

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(71) Applicant: Sumitomo Electric Industries, Ltd.
Osaka 541 (JP)

(72) Inventors:

- Nitto, Fumiaki,
c/o Itami Works
Itami-shi, Hyogo (JP)
- Sano, Tatsuya,
c/o Itami Works
Itami-shi, Hyogo (JP)

- Sakagami, Seigou,
c/o Itami Works
Itami-shi, Hyogo (JP)
- Ibuki, Masanori,
c/o Itami Works
Itami-shi, Hyogo (JP)
- Kishimoto, Hiroya,
c/o Itami Works
Itami-shi, Hyogo (JP)

(74) Representative: Eder, Eugen, Dipl.-Ing.
Patentanwälte
Dipl.-Ing. E. Eder
Dipl.-Ing. K. Schieschke
Elisabethstrasse 34
D-80796 München (DE)

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EUROPEAN SEARCH REPORT

Application Number
EP 95 11 4001

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
Y	GB-A-2 268 502 (FERODO LTD) * page 2, line 14 - page 3, line 16; examples I,II *	1-3	F16D65/02 F16D69/02
Y	DATABASE WPI Derwent Publications Ltd., London, GB; AN 83-08133k & JP-A-57 200 477 (TEIJIN KK) , 8 December 1982 * abstract *	1-3	
Y,D	DATABASE WPI Derwent Publications Ltd., London, GB; AN 87-060591 & JP-A-62 015 281 (SUMITOMO ELECTRIC IND. KK) * abstract *	1-3	

TECHNICAL FIELDS SEARCHED (Int.Cl.6)			
F16D			
<p>The present search report has been drawn up for all claims</p>			
Place of search	Date of completion of the search	Examiner	
THE HAGUE	1 March 1996	Boulon, A	
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document			
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